### Fatigue and Fracture of Materials

Wole Soboyejo and Jing Du African University of Science and Technology Abuja ((AUST Abuja) Department of Mechanical and Aerospace Engineering Princeton Institute of Science and Technology of Materials Princeton University

### Fatigue and Fracture



### **Objectives of Course**

- This course presents a graduate level introduction to fatigue and fracture of materials
- The mechanisms and mechanics and fatigue and fracture are introduced
- These are integrated with basic concepts in finite element modeling and simulations
- The frontiers of research are also presented at the end of the course

# **Course Outline**

- <u>Tuesday 6 September</u>
  - Introduction to Mechanical Properties
  - Introduction to Elasticity
  - Introduction to the Finite Element Method
  - Abaqus Software Installation and Configuration

### Wednesday 7 September

- Introduction to Plasticity
- Introduction to Notches and Fracture Mechanics
- Review of Truss Problems
- Finite Element Modeling of Truss Problems

# **Course Outline**

- <u>Thursday 8 September</u>
  - Fracture and Toughening of Materials
  - Fundamentals of Fracture Mechanics
  - Finite Element Modeling of Plate With Hole
- Friday 9 September
  - Fundamentals of Fracture Mechanics cont
  - Introduction to Fatigue
  - Finite Element Modeling of Crack Problems

## **Course Outline**

- <u>Saturday 10 September</u>
  - Case Study of Contact
  - Case Study of Adhesion
  - Finite Element Modeling of Hertzian Contact and Research Discussions

### Approach to the Course

- Intensive combination of lectures and hands on computer-based modules
- Lecture
- Break
- Lecture
- Lunch
- Finite element modeling lecture
- Finite element modeling

#### **Definitions of Stress and Strain**

- The mechanical properties of materials describe their characteristic responses to applied loads and displacements
- However, most texts relate mechanical response/behavior to stress and strain
- We will, therefore, begin with some basic definitions of stress and strain
- We will begin with simple definitions and proceed to more rigorous definitions

#### **Basic Definitions of Stress**

 The forces applied to a body may be resolved into components that are perpendicular or parallel to the surface of the body

• Axial stress =  $\sigma = \frac{\text{Applied load}}{\text{Cross-Sectional area}} = \frac{P_n}{A}$ 

• Shear stresses = 
$$\tau = \frac{\text{Applied load (Parallel to Surface)}}{\text{Cross-Sectional area}} = \frac{P_5}{A}$$

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Simple Tension

Simple Compression

Pure Shear

#### More Rigorous Definitions of Stress

- More rigorous definitions of stress are needed when the crosssectional areas are not uniform
- Uniaxial axial and shear stresses defined as the limits of the following expressions as  $dA \rightarrow 0$

$$\sigma = \lim_{dA \to 0} \left(\frac{P_n}{dA}\right)$$

and

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$$\tau = \lim_{dA \longrightarrow 0} \frac{(P_s)}{dA}$$

#### Stress as a Tensor Quantity

- Stress is not a vector quantity that can be defined by magnitude and direction of the force
- Definition must also specify area normal to the element
- Stress is a second order tensor that requires the specification of two direction normals

#### Stress on an Element



#### State of Stress and Sign Convention

- There are nine stress components on the faces of the cube.
- Special sign convention is used to define the directions of stresses that act on an element
  - first suffix, i, in  $\sigma_{ij}$  or  $\tau_{ij}$  terms corresponds to the direction of the normal to the plane
  - second suffix, j, corresponds to the direction of the load

State of Stress on an Element



#### **Stress Tensor for a Generalized Three-Dimensional Stress State**

 In the Cartesian coordinate system – the complete stress tensor for a generalized 3-D stress state is given by

 $\begin{bmatrix} \sigma_{XX} & \tau_{XY} & \tau_{XZ} \\ \sigma \end{bmatrix} = \begin{bmatrix} \tau_{YX} & \sigma_{YY} & \tau_{YZ} \\ \tau_{ZX} & \tau_{ZY} & \sigma_{ZZ} \end{bmatrix}$ 

In the cylindrical and spherical coordinate systems

Cylindrical Coordinates

$$[\sigma] = \begin{bmatrix} \sigma_{rr} & \tau_{r\theta} & \tau_{rL} \\ \tau_{\theta r} & \sigma_{\theta\theta} & \tau_{\theta L} \\ \tau_{Lr} & \tau_{L\theta} & \sigma_{LL} \end{bmatrix}$$

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Spherical Coordinates

$$[\sigma] = \begin{bmatrix} \sigma_{rr} & \tau_{r\theta} & \tau_{r\phi} \\ \tau_{\theta r} & \sigma_{\theta \theta} & \tau_{\theta \phi} \\ \tau_{or} & \tau_{\phi \theta} & \sigma_{\phi \phi} \end{bmatrix}$$

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#### Choice of Coordinate System and Some General Observations on Stress on an Element

- This depends on the geometry of the solid that is being analyzed.
- Example will choose cylindrical coordinate system in the analysis of a cylinder or body with cylindrical symmetry
- Note that there are only 6 independent stress components in any of the coordinate systems
- three axial components
- three shear components

#### **Basic Definitions of Strain**

- Applied loads or displacements result in changes in the shape of a solid
- Axial and shear strains can be defined as

 $\epsilon = U/I_0$ 

$$\gamma = w/l = tan \theta$$

Axial Strain





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#### More Rigorous Definitions of Strain

- Earlier definitions assume that stresses are uniform across area elements
- We may also define three axial strains ( $\epsilon_{xx}$ ,  $\epsilon_{yy}$ ,  $\epsilon_{zz}$ ) and three shear strains ( $\gamma_{xy}$ ,  $\gamma_{yz}$ ,  $\gamma_{zx}$ ) in 3-D state of strain



#### **Accounting for Rotation Terms**

- For stress-induced deformation we subtract out the rotation terms to describe local changes in shape
- Average rotation about x-y plane is given by

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$$\vartheta_{\mathbf{X}\mathbf{Y}} = \frac{1}{2} \left( \frac{\partial \mathbf{v}}{\partial \mathbf{x}} - \frac{\partial \mathbf{u}}{\partial \mathbf{y}} \right)$$

#### Rotation About z-Axis



#### **Basic Expressions for Rotation Components**

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• May obtain  $\omega_{yz}$  and  $\omega_{zx}$  by cyclic permutations of the (x,y,z) terms and corresponding u,v,w displacement terms

$$\omega_{yz} = \frac{1}{2} \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \qquad \qquad \omega_{zx} = \frac{1}{2} \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right)$$

• The components of the rotation matrix are given by

$$\begin{bmatrix} \omega_{ij} \end{bmatrix} = \begin{bmatrix} 0 & \omega_{xy} & \omega_{xz} \\ \omega_{yx} & 0 & \omega_{yz} \\ \omega_{zx} & \omega_{zy} & 0 \end{bmatrix} = \begin{bmatrix} 0 & \frac{\partial u}{\partial y} - \frac{\partial v}{\partial x} & \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \\ \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} & 0 & \frac{\partial v}{\partial z} - \frac{\partial w}{\partial y} \\ \frac{\partial w}{\partial x} - \frac{\partial u}{\partial z} & \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} & 0 \end{bmatrix}$$

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#### Strain Matrix for Stress-Induced Deformation

Subtracting the rotation matrix from the original strain matrix now gives

$$\begin{bmatrix} \varepsilon_{xx} & \varepsilon_{xy} & \varepsilon_{xz} \end{bmatrix} = \begin{bmatrix} \varepsilon_{xx} & \varepsilon_{xy} & \varepsilon_{xz} \end{bmatrix} = \begin{bmatrix} \frac{\partial u}{\partial x} & \frac{1}{2} \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \frac{1}{2} \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \end{bmatrix} \\ \begin{bmatrix} \varepsilon_{yx} & \varepsilon_{yy} & \varepsilon_{yz} \end{bmatrix} = \begin{bmatrix} \frac{\partial u}{\partial x} & \frac{1}{2} \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) & \frac{\partial v}{\partial y} & \frac{1}{2} \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \end{bmatrix} \\ \begin{bmatrix} \varepsilon_{zx} & \varepsilon_{zy} & \varepsilon_{zz} \end{bmatrix} = \begin{bmatrix} \frac{1}{2} \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial y} \right) & \frac{\partial v}{\partial y} & \frac{1}{2} \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \end{bmatrix} \\ \frac{1}{2} \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) & \frac{1}{2} \left( \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) & \frac{\partial w}{\partial z} \end{bmatrix}$$

- Sign convention is similar to that for stress
  - first term in  $\epsilon_{ij}$  corresponds to the direction of the normal to the plane
  - second term corresponds to the direction of the displacement induced by the applied strain

#### **Tangential Strain Components in Engineering Problems**

- The factor 1/2 often not included in several engineering problems where only a few strain components are applied
- The tensorial strains ( $\epsilon_0$  terms) are then replaced by tangential shear strain terms ( $\gamma_0$  terms) that are given by

ij =2εij

• The strain matrix for stress-induced deformations is then given by

$$\begin{bmatrix} \gamma_{ij} \end{bmatrix} = \begin{bmatrix} 0 & \gamma_{xy} & \gamma_{xz} \end{bmatrix} = \begin{bmatrix} 0 & \frac{\partial u}{\partial y} & \frac{\partial v}{\partial x} & \frac{\partial u}{\partial z} & \frac{\partial w}{\partial x} \\ \gamma_{yx} & 0 & \gamma_{yz} \\ \gamma_{zx} & \gamma_{zy} & 0 \end{bmatrix} = \begin{bmatrix} \frac{\partial v}{\partial x} & \frac{\partial u}{\partial y} & 0 & \frac{\partial v}{\partial z} & \frac{\partial w}{\partial y} \\ \frac{\partial w}{\partial x} & \frac{\partial u}{\partial z} & \frac{\partial w}{\partial z} & \frac{\partial v}{\partial z} & 0 \end{bmatrix}$$

Above shear strain components often important in plastic flow problems.

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#### The Importance of the Different Strain Components

- Tangential strain components often important in problems involving plastic flow
- Axial strain components and volumetric strain important in brittle fracture (bond rupture) problems

 $\varepsilon_{\rm Y} = \frac{\Delta V}{V} = \varepsilon_{\rm XX} + \varepsilon_{\rm yy} + \varepsilon_{\rm ZZ}$ 

Basic Definition of Volumetric Strain



#### Measurement of Local Strains from Grid Displacements

- Local strains and rotations can be measured from grid displacements
- Basic ideas are guite simple simply measure displacements and use equations to find strain/rotation component
- Resolution in displacement measurements is the key

#### Schematic of Grid Displacement Method





#### **Limitations of Small Strain Formulations**

- Above definitions apply to cases where the displacements are small.
- Large scale formulations are needed when displacements are large e.g. Lagrangian strain formulations

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$$\begin{split} \eta_{xx} &= \frac{\partial u}{\partial x} + \frac{1}{2} \left( \left( \frac{\partial u}{\partial x} \right)^2 + \left( \frac{\partial v}{\partial x} \right)^2 \right) \\ \eta_{yy} &= \frac{\partial v}{\partial y} - \frac{1}{2} \left( \left( \frac{\partial v}{\partial y} \right)^2 + \left( \frac{\partial u}{\partial y} \right)^2 \right) \\ \eta_{yy} &= \frac{1}{2} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + \frac{1}{2} \left( \frac{\partial u}{\partial x} \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \frac{\partial v}{\partial y} \right). \end{split}$$

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#### Summary and Concluding Remarks

Basic introduction to stress and strain presented along with their limitations/applications

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- Simple definitions were followed by more rigorous descriptions.
- Components of the stress and strain tensors were presented (3 axial and 3 shear terms)
- Deformation-induced strains terms were obtained by subtracting rotations from overall strains
- Tangential strain terms were defined important in engineering problems involving plastic flow

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• Lagrangian strain formulation presented for larger displacements